# Gravity From a Buried Sphere

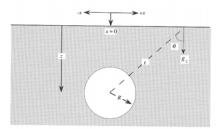


Figure 6-13 Notation used in derivation of the gravity effect of a buried sphere. The same notation is used for a traverse at right angle to the strike of a horizontal, infinitely long cylinder.

# Gravity from a Sphere

excess mass due to the sphere is equal to  $4\pi R^3 p_c/3$ . Using Eq. 6-4 we see that the gravitational attraction of the sphere in the direction of r is

$$g_{sphere(r)} = \frac{Gm}{r^2} = \frac{G4 \pi R^3 \rho_e}{3r^2} = \frac{G4 \pi R^3 \rho_e}{3(x^2 + z^2)}$$
(6-33)

We seek the vertical component of  $g_{upanter}$ , because gravimeters respond only to gravity in the vertical direction. In general, unless noted otherwise, the component in the vertical direction  $g_i$  is implied. Therefore,

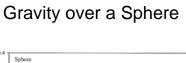
$$g_{sphore} = \frac{G4 \pi R^3 \rho_c}{3(x^2 + z^2)} \cos \theta = \frac{G4 \pi R^3 \rho_c}{3} \frac{z}{(x^2 + z^2)^{1/2}}$$
 (6-34)

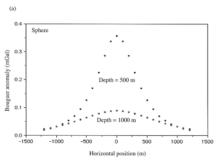
Now that we have the required equation, let's study some attributes of gravity over a buried sphere. Table 6-6 uses Eq. 6-34 and allows us to directly compare gravity over two spheres, so we can vary parameters in each and observe the differences. In case you are interested in making similar computations for other equations we present, Eq. 6-35 illustrates units conversion, so g is in mGal when density is in  $g/cm^3$ , distances are in meters, and G is in dyne  $^*$  cm $^3/g^3$ .

$$g(mGal) = 6.67 \times 10^{-8} \, \frac{dyne \, cm^2}{g^2} \cdot \frac{g}{cm^3} \cdot \frac{m}{1} \cdot \left( \frac{g \, cm \, /s^2}{dyne} \cdot \frac{100 \, cm}{m} \cdot \frac{gal}{cm \, /s^2} \cdot \frac{1000 \, mGal}{Gal} \right)$$

## Gravity over a Sphere

Sphere A			Sphere B
Sphere radius (m) Depth to sphere center (m) Density contrast (g/cm3) Horizontal increment	200 500 0.4 100	Sphere radius (m) Depth to sphere center (m) Density contrast (g/cm3) Horizontal increment	200 1000 0.4 100
Horizontal Position (m)	Gravity (mGal)	Horizontal Position (m)	Gravity (mGal
-1200	0.0203	-1200	0.0235
-1100	0.0253	-1100	0.0272
-1000	0.0320	- 1000	0.0316
- 900	0.0410	- 900	0.0367
- 800	0.0532	- 800	0.0426
- 700	0.0702	- 700	0.0492
- 600	0.0938	- 600	0.0564
- 500	0.1264	- 500	0.0640
- 400	0.1703	- 400	0.0716
- 300	0.2255	- 300	0.0786
- 200	0.2862	- 200	0.0843
- 100	0.3372	- 100	0.0881
0	0.3576	0	0.0894
100	0.3372	100	0.0881
200	0.2862	200	0.0643
300	0.2255	300	0.0786
400	0.1703	400	0.0716
500	0.1264	500	0.0640
600	0.0938	600	0.0564
700	0.0702	700	0.0492
800	0.0532	800	0.0426
900	0.0410	900	0.0367
1000	0.0320	1000	0.0316
1100	0.0253	1100	0.0272
1200	0.0203	1200	0.0235





# Gravity Effect of a Horizontal Cylinder

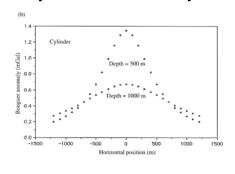
Figure 6-13 equals  $\pi R^2$ , substituting into Eq. 6-20 gives us, for gravity in the direction of r,

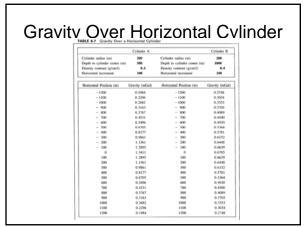
$$g_{cylinder(r)} = \frac{G 2 \pi R^2 \rho_c}{r}$$
(6-36)

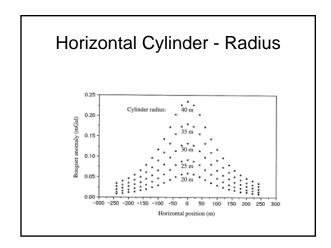
$$g_{\text{cylinder}} = \frac{G2 \pi R^2 \rho_c}{r} \cos \theta = \frac{G2 \pi R^2 \rho_c z}{r^2}$$

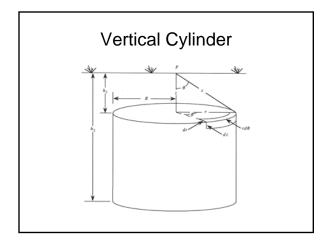
$$g_{\text{cylinder}} = G2 \pi R^2 \rho_c \frac{z}{\left(x^2 + z^2\right)}$$
(6-3)

# Gravity of a Horizontal Cylinder









## Vertical Cylinder

$$\Delta g_{\text{section clotherry}} = \frac{G\rho_{r}dz (rd\phi) dr}{z^{2}}$$

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$$\Delta g_{\text{section clotherry}} = \frac{G\rho_{r}dz (rd\phi) dr}{z^{2}}$$

$$z = \frac{G\rho_{r}dz (rd\phi) dr}{z^{2}}$$
(6-38)

$$\Delta g_{restiral collision} = \frac{G \rho_c(zdz)(rdr) d\phi}{\int_{-2}^{2} \frac{1}{r^2} \sqrt{r^2}}$$
(6-39)

 $\Delta g_{\rm resind c (sinher)} = \frac{G \rho_c (zdz) (rdr) d \phi}{(r^2 + z^2)^{3/3}} \tag{6-39}$  Next we determine the gravitational attraction of the cylinder by using the volume element to sweep out a thin ring, then a thin disc, and finally the cylinder. Equation 6-40 gives the formula for this integration.

$$g_{serical cylinder} = \int_{s_1}^{s_2} dz_0^F \int_0^{2\pi} \frac{G\rho_r(z)(r)}{(r^2 + z^2)^{3/2}} d\phi$$
 (6-40)

The result of this integration is Eq. 6-41.

$$g_{retrical cylinder} = G 2 \pi \rho_c \left( h_2 - h_1 + \sqrt{R^2 + h_1^2} - \sqrt{R^2 + h_2^2} \right)$$
 (6-41)

Note that this equation gives gravity only at a point above the cylinder axis and is not valid for determining gravity at points away from the axis.

# Vertical Cylinder -> Terrain

There are some other interesting results that arise from this derivation. When evaluating the integral from 0 to R, if we assume R goes to infinity, the result is an equation for an infinite slab (the Bouguer correction). Hence, we could have used this approach to determine the Bouguer correction. In addition, if we have a large cylinder with radius R0 and a smaller cylinder (with radius R0 with an axis coincident with the larger cylinder and with coincident to and betonen, we can determine the effect of a ring by subtracting the effect of the smaller cylinder from the larger. Let P be on the top of the cylinder, so that  $h_1 = 0$ , and let the bottom of the cylinder be a distance; from the top, then

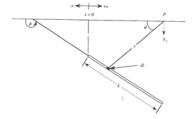
$$g_{\text{risg}} = G2\pi\rho_{c}\left[\left(z + \sqrt{R_{o}^{2}} - \sqrt{R_{o}^{2} + z^{2}}\right) - \left(z + \sqrt{R_{i}^{2}} - \sqrt{R_{i}^{2} + z^{2}}\right)\right]$$

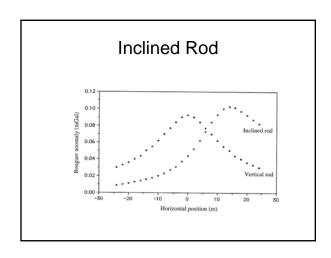
$$g_{ring} = G2\pi\rho_i \left(R_o - R_i - \sqrt{R_o^2 + z^2} + \sqrt{R_i^2 + z^2}\right).$$
 (6-42)

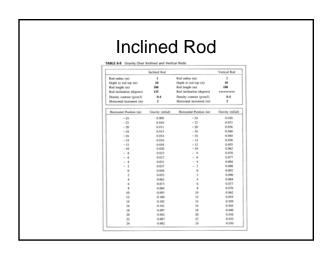
Equation 6-42 is the terrain correction.

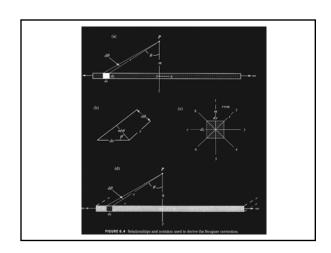
## Inclined Rod

$$g_{revival \, rod} = G \rho_r \pi R^2 \left\{ \frac{1}{\left(z^2 + x^2\right)^{1/2}} - \frac{1}{\left[\left(z + L\right)^2 + x^2\right]^{1/2}} \right\}$$
 (6-43)









# Gravity Due to an Infinite Rod

The attraction of a thin rod is the sum of all these components, so we write

$$g = \int_{z=-\infty}^{z=\infty} \frac{G(\rho dxdydz)}{r^2} \cos\theta. \qquad (6.18)$$

Before evaluating the integral, we note that  $r=m/\cos\theta$ . Also (see Figure 6.4(b)), because the length of arc for a small angle  $d\theta$  equals the radius r times the change in angle  $d\theta$ , it is straightforward to demonstrate that  $dx=r\,d\theta/\cos\theta$ . Using these relationships, we show that

 $\frac{G(\rho d\nu d\nu dz)}{r^2}\cos\theta = \frac{G(\rho d\nu dz)rd\theta\cos\theta(\cos\theta)^2}{m^2\cos\theta} = \frac{G(\rho d\nu dz)rd\theta\cos\theta(\cos\theta)^2}{m^2\cos\theta\cos\theta} = \frac{G(\rho d\nu dz)}{m}\cos\theta$ 

Using this result, we adjust Equation 6.18 so that

$$g = \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} \frac{G(\rho dy dz)}{m} \cos \theta \ d\theta \tag{6.19}$$

which evaluates to

$$g = \frac{2G\rho dydz}{m}.$$
 (6.2)

Equation 6.20 gives us g at P over a thin rod as illustrated in Figure 6.4(a)

# Gravity Due to an Infinite Slab

The next step in our derivation is to sweep out a thin sheet using a thin rod (that is, use Equation 6.20 to calculate g over a thin sheet). Figure 6.4(c) is an end view of our thin rod. If lines 1, 2, 3, 4, 5, 6, 7, and 8 are of equal length, then g is the same at the end of every line. Line 1 is equivalent to m in our original diagram, and we will refer to line 2 as r. Clearly m = r and g is the same at positions 1 and 2. This gives us the same view of the thin rod as we see in Figure 6.4(d), where line 2 now is labelled as r. Because we know g due to the thin rod (Equation 6.20), we use this to write

$$\Delta g_r = \frac{2G(\rho dydz)}{r}.$$
 (6.21)

The next several steps mimic exactly those that we just listed, so following the same procedure we can say that  $\,$ 

$$\Delta g_z = \frac{2G(\rho dydz)}{r}\cos\theta \tag{6.22}$$

$$g = \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} 2G(\rho dz)d\theta \qquad (6.23)$$

and

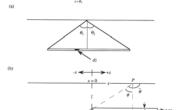
 $g = 2\pi G(\rho dz). \tag{6.24}$ 

## **Horizontal Sheet**

#### Gravity Effect of a Horizontal Sheet

When deriving the Bouguer effect, we created a thin slab by moving a thin rod from  $+\infty$  to  $-\infty$  (integrating from  $\pi/2$  to  $-\pi/2$ ; see Eq. 6-23). If instead we integrate from  $\theta_i$  to  $\theta_2$  (see Fig. 6-19(a)), we have

$$g = \int_{z=0}^{z=\theta_2} 2G(\rho dz) d\theta \qquad (6-44)$$



## **Horizontal Sheet**

$$g = 2 G \rho_c \left( dz \overline{\theta} \right)$$
 (6-45)

where  $\overline{\theta}$  represents the included angle in radians. If we keep the slab thin with respect to its depth, we can write

$$r_{ancuted slab} = 2 G \rho_c t (\overline{\theta}) \qquad (6-46)$$

 $g_{tremonfolds} = 2 \, Gp, t[\overline{\theta}] \qquad (6-46)$  where t is the thickness of the truncated slab (Fig. 6-19(a)). Our goal in this section is to derive a relationship for a semi-infinite slab (Fig. 6-19(b)). For this case the included angle  $\theta$  is equal to  $\pi/2 + \tan^{-1}(\nu/2)$  and we therefore have

$$g_{semi-sheer} = 2 G \rho_c t \left( \frac{\pi}{2} + \tan^{-1} \frac{x}{z} \right)$$
 (6-47)

This approximation is within 2 percent if  $z \ge t$  (Telford et al. 1990, p. 40). Table 6-9 uses

## **Horizontal Sheet**

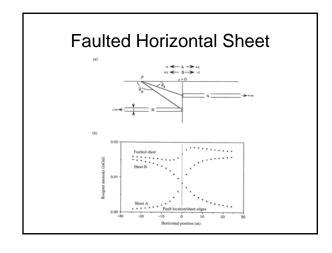
	Short A		Sheet B
Depth to short (m)	4	Depth to sheet (m)	
Short thickness (m)	1	Short thickness (m)	1
Density contrast (gicm3)	0.4	Density contrast (g/cm2)	9.4
Horizontal increment (m)	2	Horizontal increment (m)	2
Horizontal Position (m)	Gravity (mGal)	Horizontal Position (m)	Granity (mGal
24	0.0009	-24	0.0150
22	0.0010	-22	0.0049
20	0.0011	-20	0.0647
18	0.0012	-18	0.0045
16	0.0013	-16	0.0043
14	0.0015	-14	0.0040
12	0.0017	-12	0.0036
10	0.0030	-10	0.0132
	0.0025	- 8	0.0026
6	0.0031	- 6	0.0118
4	0.0042	- 4	0.0009
2	0.0059	- 2	0.0097
	0.0084	0	0.0064
- 2	0.0009	2	0.0071
- 4	0.0126	4	0.0059
- 6	0.0136	6	0.0049
- 8	0.0143		0.0042
-10	0.0147	10	0.0056
-12	0.0150	12	0.0051
-14	0.0153	14	0.0028
-16	0.0155	16	0.0025
-18	0.0156	18	0.0022
-20	0.0157	20	0.0000
-22	0.0158	22	0.0019
-24	0.0159	24	0.0017

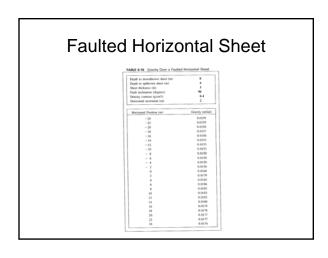
## Faulted Horizontal Sheet

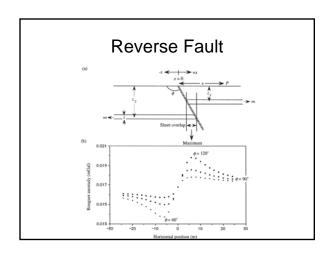
The equation for the faulted horizontal sheet is

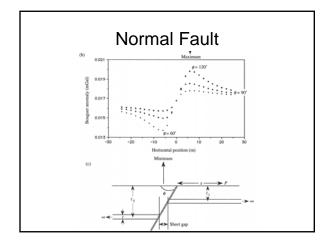
$$g_{finhold decet} = 2 G \rho_c I \left[ \pi + \tan^{-1} \left( \frac{x}{z_1} + \cot \phi \right) - \tan^{-1} \left( \frac{x}{z_2} + \cot \phi \right) \right]$$
 (6-48)

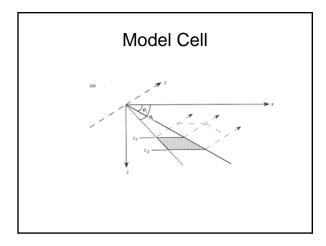
 $g_{fambat deser} = 2 G \rho_z I_{\pi} + \tan^{-d} \left( \frac{x}{z_t} + \cot \phi \right) - \tan^{-d} \left( \frac{x}{z_0} + \cot \phi \right) \right]$  (6-48) where x is the horizontal position of the measurement location, x is sheet thickness,  $\phi$  is fault inclination, x, is depth to uphrown block, and z, is depth to downthrown block. Note that the relative positions of the faulted sheet are constant (i.e., the upthrown block is always











# Model Cell

lowing a procedure much like we employed to determine the Bouguer correction, the semi-infinite sheet, and the vertical cylinder. If we have a small cell of infinite length in the  $\hat{y}$ -idimension with side lengths  $d\hat{z}$  and  $d\theta$ , the gravity effect of such a cell is easily determined by integration. Thus, we have

$$g_{cell} = 2 G \rho_c \int_0^{\theta_2} d\theta \int_0^{z_2} dz$$

$$g_{cell} = 2 G \rho_c (\theta_2 - \theta_1) (z_2 - z_1) \qquad (6-50)$$

The notation is defined in Figure 6-22(a). All we need now do is to represent a polygon such as that illustrated by Figure 6-22(b) as an accumulation of such cells. If a polygon has n such cells, then the gravity effect of the polygon is

$$g_{polygon} = 2 G \rho_c n \Delta \theta \Delta z$$
 (6-51)

